QPE 233

Non-Negative K_{DP} **Estimation by Monotone** Increasing Φ_{DP} Assumption below Melting Layer



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INTRODUCTION

A specific differential phase (K_{DP}) is a powerful dual-polarimetric parameter for QPE. The K_{DP} is not directly observed by radar system, but is calculated by a derivative of a differential phase (Φ_{DP}) with respect to range. Because the observed Φ_{DP} is contaminated by noise, and the differentiation works as a high-pass filter, it is difficult to retrieve the original K_{DP} . Thus local linear or polynomial regression are generally used to estimate the K_{DP} ; however, these procedures make a spatial resolution of the K_{DP} coarse. Furthermore, a differential backscatter phase (δ) overlaps in the observed Φ_{DP} .

In this paper, a new K_{DP} estimation method is proposed by assuming the monotone increasing Φ_{DP} below melting layer. The K_{DP} estimated by this method always takes a positive value.

Schematic range profiles of the observed and analyzed Φ_{DP} in this method. Horizontal and vertical axes indicate the range from radar and the differential phase, respectively. Dots indicate the observed differential phase (Ψ) at the range, and blue solid curve is a final solution of the differential phase in this method. Broken red lines are boundary conditions of the differential phases (Φ_{near} and Φ_{far}) at the nearest and farthest ranges (r_{near} and r_{far}), respectively. Lines LR-N and LR-F are linear regression lines to determine the boundary conditions (Φ_{near} and Φ_{far}), respectively. ϕ and ψ (ϕ' and ψ') indicate the difference from the nearest (farthest) boundary condition, respectively.





METHOD

1. Quality Control

At first, the observed data in or higher than melting layer should be rejected, because this method is only available for pure rainfall. Of course, a precipitation particle identification can be used by using the dual-polarimetric information; however it is not completely robust at present. The zero degree level information from sounding data or numerical simulations, and the assumed melting layer depth (e.g., 500 m or 1000 m) may be useful for this purpose.

Then no precipitation (low S/N ratio) data, ground and point clutter data, and outlier data are rejected. Finally $\Phi_{\rm DP}$ unfolding should be performed in case the Φ_{DP} exceeds a expression range of 360 ° or 180 °.

2. Boundary Conditions

This method needs two boundary conditions: the nearest and farthest Φ_{DP} $(\Phi_{\text{near}} \text{ and } \Phi_{\text{far}})$. The final solution of Φ_{DP} varies between these boundary conditions.

The nearest boundary Φ_{near} is determined by the linear regression (Line LR-N in schematic profile above), which is calculated with the specified number (e.g., 30) of available data from the nearest range. If the slope of the regression line is positive, the value of the regression line at the nearest range (r_{near}) is used for the boundary condition. Otherwise, the averaged value of the available data is used. The farthest boundary Φ_{far} is determined in the same manner (see Line LR-F in the schematic profile).

3. Cost Function

Now the observed and final solution of differential phase are denoted as Ψ_i and $(\Phi_{DP})_i$, respectively, where the suffix i is an index of range (i = 0, 1, 2, ..., N). Here we define ϕ_i as,

 $\phi_i = (\Phi_{\rm DP})_i - \Phi_{\rm near}.$ This ϕ_i can be written with K_{DP} as, $\phi_0 = 0,$

$$\phi_i = 2\sum_{j=0} (K_{ ext{DP}})_j \Delta r \qquad (i=1,2,3,\cdots,N).$$

1x10¹⁰)

 \bigcirc Dependency of the C_{lof} to the low pass filter in this method. The details of this figures are the same as above. a) $C_{lof} = 0$, b) $C_{lof} =$ 1×10^8 , c) $C_{lof} = 1 \times 10^9$, d) $C_{lof} = 1 \times 10^{10}$, e) $C_{lof} = 1 \times 10^{11}$, and f) $C_{lof} =$ 1×10^{12} . Left and right panels are K_{DP} and Φ_{DP} , respectively.

Because we assume that K_{DP} always takes a positive value, we introduce k_i as,

$$k_i^2 = 2(K_{
m DP})_i \Delta r.$$

So (3) can be written with k_i as,

$$\phi_i = \sum_{j=0}^{i-1} k_j^2$$
 $(i = 1, 2, 3, \dots, N).$

On the other hand, the reverse version of ϕ_i is also defined as,

$$\phi'_i = \Phi_{\text{far}} - (\Phi_{\text{DP}})_i.$$

This ϕ'_i can be written with k_i as,

(a) Reflectivity

$$\phi'_i = \sum_{j=i+1}^N k_j^2$$
 $(i = 0, 1, 2, \dots, N-1),$
 $\phi'_N = 0.$

The differences between observation and the boundaries are also defined as,

 $\psi_i = \Psi_i - \Phi_{\text{near}},$ $\psi'_i = \Phi_{\text{far}} - \Psi_i.$

Hear a cost function (with respect to k) to be minimized is defined as,

$$J = J_{obs} + J'_{obs} + J_{lpf}, \qquad (11)$$

$$J_{obs} = \frac{1}{N} \sum_{i=1}^{N} (\phi_i - \psi_i)^2, \qquad \text{Mean Square Errors of}$$

$$J'_{obs} = \frac{1}{N} \sum_{i=0}^{N-1} (\phi'_i - \psi'_i)^2, \qquad \text{Mean Square of Laplacian of k,}$$

$$J_{lpf} = \frac{1}{N+1} C_{lpf} \sum_{i=0}^{N} \left(\frac{\partial^2 k_i}{\partial r^2}\right)^2. \qquad \text{Mean Square of Laplacian of k,}$$

$$Worked as a Low-Pass Filter$$

 J_{obs} and J'_{obs} make the analyzed differential phase fitted to the observed one. J_{lof} works as a low pass filter. C_{lof} is a control parameter of the low pass filter.

We regard the range profile of k which minimizes the cost function as the final solution in this problem. The final K_{DP} is calculated from k by (4).

(b) Differential phase

COMPUTATION COST

To minimize the cost function, we use the Broyden-Fletcher-Goldfarb-Shanno (BFGS) method, which is a kind of numerical optimizations. Because the BFGS method is described by a recurrence formula, a numerical iteration must be performed to suffer from a heavy computation cost. In typical rainfall case, it takes several hundred milliseconds to solve the K_{DP} range-profile of one ray. So it is difficult to embed this method in the radar signal processor.

Fortunately, an inexpensive parallel computing is now available. We can calculate the whole K_{DP} in one PPI scan in 10 seconds to 15 seconds. This means that this method is acceptable for the operational use.

Radar Data	
Radar Frequency	X-band (9375 MHz)
Number of range bins / ray	801
Number of rays / PPI	360
Max. range	80 km (100 m x 800)
Computer	
CPU	Intel Xeon E5630
	(2.53 GHz, 4 cores)
Number of CPUs / node	2
OS	CentOS 5.5
Communication	1000Base-T
Parallelization	MPI
Calculation Time	
Number of processes	Cal time (see)

97.38

23.32

12.38

8.59



example of the minimizing of the cost function by BFGS method. Colors of plots correspond to the colors of K_{DP} and Φ_{DP} profiles shown below.



1 (1 node)

8 (1 node)

16 (2 node)

24 (3 nodes)

 K_{DP} profile modifications at each BFGS iteration step. Colors of the profiles correspond to the color plots shown in upper right.

 Φ_{DP} profile modifications at each BFGS iteration step. Colors of the profiles correspond to the color plots shown in upper right.

CASE STUDY (Heavy Precipitation on 10 May 2012)

(c) K_{DP} (NIED stable)

(1)

(2)

(3)

(4)

(5)

(6)

(7)

(8)

(9 and 10)





PPI images of NIED's X-band polarimetric radar at Ebina city at 0500 UTC 10 May 2012. The elevation angle is 1.2. Range circles are drawn at 20 km intervals from the radar. a) Observed reflectivity (no attenuation correction), b) Observed differential phase, c) Specific differential phase estimated by classic method (NIED stable algorithm: the iterative filter and local linear regression; the data which S/N ratio less than 10 dB are not used.), d) Specific differential phase estimated by this method ($C_{lof} = 1 \times 10^{10}$), and e) Rainfall rate calculated from K_{DP} shown in (f).

Probability density of scatter plots of Z_h versus K_{DP} calculated by this method (C_{lof} =1x10¹⁰). The data are observed by NIED's X-band dual-pol. radar at 1402 UTC 9 July 2005.